ENHANCED PROPERTIES OF HYPERBRANCHED POLYURETHANE ELASTOMERS BASED ON POLYDIMETHYLSILOXANE/POLYETHER MIXED SOFT SEGMENTS

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ABSTRACT

A novel hydroxyl-terminated polymer HPMS-APE was synthesized by introducing allyl polyethylene oxide (APE) into hydrogen-terminated polydimethylsiloxane (HPMS) backbone by hydrosilylation reaction. A series of hyperbranched polyurethane elastomers (HBPUs) based on HPMS-APE and polypropylene glycol (PPG) mixed soft segments were successfully synthesized with trimethylolpropane (TMP) as a chain extender. The effect of HPMS-APE segments content on enhanced properties of HBPUs were characterized by Fourier transform infrared spectroscopy (FT-IR), differential scanning calorimetry (DSC), atomic force microscopy (AFM), thermogravimetric analysis (TGA), mechanical testing and water absorption. It was found that incorporating HPMS-APE in polyurethanes made substantial changes in their morphology, thermal properties, mechanical properties and water absorption. When 5 wt% HPMS-APE was incorporated in HBPUs, the extent of microphase separation between hard and soft segments was the best, resulting in polyurethanes without significant compromise in tensile strength and elasticity. Furthermore, HBPUs derived from HPMS-APE presented excellent thermal stability and unique water resistance.

Keywords: Hyperbranched, Polydimethylsiloxane, Polyurethanes, Microphase separation

INTRODUCTION

Polyurethanes are multiblock copolymers consisting of alternate hard and soft segments. The hard segments are in a crystalline state or an amorphous glassy state giving materials stiffness and strength, while the soft segments are in a rubbery state giving the elasticity and flexibility. The unique properties of polyurethanes result from both their chemical structure and the extent of microphase separation between hard and soft segments.

Recently, to enhance properties of polyurethanes such as thermal stability, water resistance, gas permeability and biocompatibility, polydimethylsiloxanes (PDMS) are widely used for preparing copolymers with polyurethanes because of their excellent properties such as oxidative and hydrolytic stability, good blood contacting properties, a wide service temperature range due to low glass transition temperature (-123 °C), low moisture permeability and low surface energy.

However, it has been identified that the major problem associated with synthesizing PDMS-based polyurethanes is the large difference between the solubility parameter of the nonpolar PDMS segments and high polar urethane hard segments, where PDMS as soft segments demonstrates excess degree of microphase separation, yields relatively poor mechanical properties. Therefore, a number of methods have been confirmed to improve the phase mixing of these materials. The main approaches reported were to introduce polar functionality into PDMS backbone, or to use blended soft segments of PDMS and polyether-diol. At present, some researchers have reported related copolymers, but they mainly concentrate on the studies of linear polyurethanes. For example, Adhikari et al. have demonstrated that when a relatively small amount of a second macrodiol was incorporated as part of the soft segments along with PDMS in linear polyurethanes, the compatibility of the PDMS soft and urethane hard segments could be significantly improved. Lee and coworkers have reported that the PDMS/polyether mixed soft segments linear urethane membranes had well-phase separated structures. However, no papers can, as yet, be found for detailed studies on properties of PDMS-based hyperbranched polyurethanes. It is known that mechanical properties of hyperbranched polyurethanes are improved by chemical crosslinking process. Hence, it is very interesting to study the properties of hyperbranched polyurethanes modified by PDMS, and it is meaningful to analyze and control bulk properties of the materials.

In this work, a novel hydroxyl-terminated polymer HPMS-APE was synthesized by introducing allyl polyethylene oxide (APE) into hydrogen-terminated polydimethylsiloxane (HPMS) backbone by hydrosilylation reaction. The chemical structure of HPMS-APE was confirmed by 1H-nuclear magnetic resonance (1H-NMR) and Fourier transform infrared spectroscopy (FT-IR). A series of hyperbranched polyurethane elastomers (HBPUs) based on HPMS-APE and polypropylene glycol (PPG) mixed soft segments were successfully synthesized with trimethylolpropane (TMP) as a chain extender. The product formed the crosslinking structures during the chain extension process. The aim of this study was to investigate the effect of HPMS-APE segments content on enhanced properties of HBPUs. The structures of HBPUs were supported by FT-IR. The morphology was investigated by differential scanning calorimetry (DSC) and confirmed by atomic force microscopy (AFM), which provided advantage evidence to the analysis and control the bulk properties. The thermal properties of HBPUs were examined by thermogravimetric analysis (TGA). In addition, the mechanical properties and water absorption were also studied.

EXPERIMENTAL

Materials

4, 4’-Methylene diphenyl diisocyanate (MDI) was received from Aladdin Chemistry Co., Ltd. and vacuum distilled before use. Polypropylene glycol (PPG, Mn = 1000) and allyl polyethylene oxide (APE, Mf = 400) were desiccated at 110 °C before use, which were supplied by Zhongshan Chemical Co., Ltd. (Jiangsu, China). Trimethylolpropane (TMP) was purchased from Sinopharm Chemical Reagent Co., Ltd. (Beijing, China). Hydrogen-terminated polydimethylsiloxane (HPMS, Mn = 1000) was self-made. Chloroplatinic acid was received from Nanjing Chemical Reagent Co., Ltd. (Jiangsu, China).

Synthesis of HPMS-APE

The synthesis of HPMS-APE is shown in Scheme 1. A stoichiometric amount of HPMS and APE (molar ratio of HPMS and APE was 1.0:2.1) with the presence of chloroplatinic acid were added in a 250 mL flask, and reacted at 120 °C for 5 h. After the reaction was completed, the mixture was distilled in vacuo at 110 °C to remove the remaining APE. It was found that the hydroxyl value and acid value of the resulting transparent HPMS-APE were 62.1 mg KOH g-1 and 0.32 mg KOH g-1, respectively.

Synthesis of HBPUs

A series of HBPUs were prepared by two-step bulk polymerization without catalyst and additives, which was outlined in Scheme 2. The corresponding compositions are shown in Table 1. All glasswares were dried in an oven overnight at 105 °C.

Prepolymer preparation: HPMS-APE and PPG were charged in a 100 mL four-necked flask equipped with a mechanical stirrer, a nitrogen inlet, a reflux condenser and a thermometer. The flask was kept at 120 °C for 2 h under vacuum to remove traces of water. When the temperature was cooled down to 40 °C, MDI was added into the flask. Then the mixture reacted at 80 °C for 2 h under N2 to obtain an isocyanate-terminated polymer having an isocyanate content of 6.5 wt%, which was quantitatively determined by the di-n-butyl amine method.

H-NMR) and Fourier transform infrared spectroscopy (FT-IR)
Scheme 1. Synthesis of HPMS-APE.

Scheme 2. Preparation of HBPUs.

Chain extension: Following the above-mentioned process, a required amount of TMP was added in the reactor at 80 °C and stirred vigorously for 2 min. Then the flask was degassed for 10 min in ultrahigh vacuum to ensure the removal of air bubbles. Finally, the mixture was cast rapidly in a preheated teflon mould to form a 1-2 mm thick sheet, and cured for 24 h at 120 °C.

Table 1. Compositions of HBPUs prepared in this study.

<table>
<thead>
<tr>
<th>Sample</th>
<th>HPMS-APE/PPG/MDI/TMP (molar ratio)</th>
<th>HPMS-APE content (wt%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>HBPU0</td>
<td>0/1.0/2.4/0.93</td>
<td>0</td>
</tr>
<tr>
<td>HBPU1</td>
<td>0.05/0.95/2.4/0.93</td>
<td>5</td>
</tr>
<tr>
<td>HBPU2</td>
<td>0.10/0.90/2.4/0.93</td>
<td>10</td>
</tr>
<tr>
<td>HBPU3</td>
<td>0.15/0.85/2.4/0.93</td>
<td>15</td>
</tr>
<tr>
<td>HBPU4</td>
<td>0.20/0.80/2.4/0.93</td>
<td>20</td>
</tr>
</tbody>
</table>

Characterization and measurements

1H-NMR spectra of HPMS-APE was recorded with a Bruker 400 MHz spectrometer in deuterated chloroform (CDCl₃) with tetramethyl silane (TMS) as an internal reference and the operating temperature was 30 °C.

FT-IR spectrum of HBPUs was measured by a FT-IR spectrometer (Nicolet 8700, Boston, MA) in the wave number of 550-4000 cm⁻¹ at 25°C. For each FT-IR spectrum sample, 32 scans were collected in the transmittance mode.

The thermal properties of HBPUs were measured by a DSC 2010 thermal analyzer (TA instrument) with a DSC module, purged with nitrogen gas, and quenched with liquid nitrogen. The specimens were scanned from -150 °C to +200 °C by a heating rate of 10 °C/min. The cell was calibrated using an indium standard. The weight of sample was 5-10 mg.

Microrheology separation in HBPUs was investigated using a Digital Instruments MultiMode AFM using tapping mode. The images were acquired under ambient conditions using light to moderate tapping.

The thermal stability of HBPUs was investigated using a TGA 2050 (TA instrument). The heating rate was 10 °C/min and heated up to 600 °C under air. The weight of sample was 5-10 mg.

The mechanical tests to determine tensile strength, elongation at break and hardness were carried out on dumbbell samples. Tensile strength and elongation at break were determined using an Instron-2380 Universal Testing Machine (Instron Corporation, USA) at a strain rate of 50 mm/min. Shore hardness was measured on a WHS-150/Shore Hardness Tester (Instron Corporation, USA).

The water absorption was determined as follows. The samples were cut in 3 cm×1 cm pieces and dried in a vacuum oven for 24 h to determine their dry weight (W_d). Then the sample was immersed in distilled water for 24 h, 48 h and 72 h, followed by wiping off the surface water with a piece of filter paper to determine their weight (W_t). The water absorption (Wₛ) was then calculated by the formula:

$$W_s = [(W_t - W_d) / W_d] \times 100\%$$ (1)
RESULTS AND DISCUSSION

'H-NMR and FT-IR spectroscopy

The chemical structure of HPMS-APE was examined by 'H-NMR and FT-IR. Figure 1 shows several characteristic 'H-NMR spectra of HPMS-APE. δ > 5 ppm did not find absorption peaks, demonstrating that there was no remaining APE in the product. As shown in Figure 2, the typical absorption peaks of polyurethanes at 3300 cm⁻¹ [ν (NH)], 2865-2965 cm⁻¹ [ν (CH₂) and ν (CH₃)], 1700-1725 cm⁻¹ [ν (C=O)], 1530 cm⁻¹ [δ (NH)] and 1070 cm⁻¹ [ν(C-O-C)] could be seen clearly in the spectra. Compared with FT-IR spectra of HBPU0 based on pure PPG segments, characteristic peaks for HPMS-APE segments in HBPU2 and HBPU4 were clearly noticed. The presence of HPMS-APE in HBPUs was demonstrated by the formation of the absorbance peaks at around 1258 cm⁻¹ [ν (CH₃) in Si-CH₃], 1000-1100 cm⁻¹ [ν (Si-O-Si)] and 801 cm⁻¹ (CH₃-Si rocking). Additionally, characteristic peaks were noticeably stronger as the content of HPMS-APE increased. Finally, FT-IR spectra of all other samples were very similar to above FT-IR results and we confirmed the synthesis of HBPUs based on HPMS-APE and PPG mixed soft segments.

DSC and AFM analysis

DSC was used to investigate the morphological effect of HBPUs with different content of HPMS-APE segments. Figure 3 shows the DSC thermograms for HBPUs. In the series, all polyurethanes showed a common melting endotherm (T_m) at around 80 °C, which was assigned to melting of hard segments region derived predominantly from MDI/TMP. The peak of T_m remained unchanged with increasing HPMS-APE content, while the heat of fusion (ΔH) for melting endotherms decreased, which was indicative of enhanced phase mixing between hard and soft segments. It was interesting to note that the ΔH was the lowest for HBPU1 with 5 wt% HPMS-APE, indicating the most phase mixing of the series. The change in soft segments glass transition temperatures (T_g) supported this.

Figure 4 shows the AFM images of HBPUs. According to the principle of tapping mode of AFM operation, the light color areas in Figure 4 represented the hard segments region, and the dark color areas correspond to the soft segments region. Figure 4a shows the AFM image of HBPU0, microphase separation between hard and soft segments can be observed clearly. The congregating hard segments dispersed into the soft phases, but the size of hard segments region was a little bit larger. Figure 4 (b, c, d, e) shows the AFM images of HBPUs with different content of HPMS-APE segments, hard segments region also dispersed into the soft phases, but the size of micro-domain became smaller, because that HPMS-APE segments which were incompatible with hard segments prevented the large hard segments region packing. From Figure 4b, the hard segments region was more dispersive into the soft phases than the others. In other words, HBPU1 showed a very well microphase separation between hard and soft segments. All those were identical with the analysis results from DSC.
Mechanical properties

To evaluate the effect of HPMS-APE segments content on the mechanical properties of HBPUs, tensile tests and Shore hardness tests were performed, as showed in Figure 6a and 6b, respectively. In all cases, the elongation at break of HBPUs gradually increased with increasing HPMS-APE content because of the flexibility of the PDMS. Hardness scores for HBPUs were within the range of 72 A to 83 A, and there was a tendency for the hardness scores to lower as the HPMS-APE content increased. However, it was noteworthy that the tensile strength remained largely unchanged up to 5 wt% of HPMS-APE, yet increasing HPMS-APE above 10 wt% made HBPUs mechanically weaker than HBPU0 based on pure PPG segments, with HBPU4 showing the lowest tensile strength of the series. Similar observations were reported by Chen21 on the effect of siloxane content on the mechanical properties of PDMS urethanes. The reasons were as follows: the mechanical properties of polyurethanes were profoundly dependent on the degree of microphase separation12, and the enhanced phase mixing between hard and soft segments resulted in the best mechanical properties of HBPU1 with 5 wt% of HPMS-APE, that was in agreement with DSC and AFM analysis. However, when increasing HPMS-APE content above 10 wt%, the tensile strength tended to decrease, resulted from the more HPMS-APE segments content, as well as the excess degree of microphase separation got the negative effect20. Compared with previous work on PDMS-based polyurethane materials, in this study, the incorporation of HPMS-APE in polyurethanes can be controlled to a certain degree, polyurethanes could be prepared without significant compromise in tensile strength and elasticity.

Thermal stability

TGA and DTG curves for HBPUs with different content of HPMS-APE are presented in Figure 5. The detailed data of $T_m$ (the temperature at 5% weight loss), $T_{max1}$ (maximum rate of degradation temperature in the first step), $T_{max2}$ (maximum rate of degradation temperature in the second step) and $W_r$ (residue at 600 °C), are summarized in Table 3. As was known, the first decomposition fraction in the polyurethane chains was the hard segments, which involved the urea and the urethane groups. Decomposition of the soft segments followed the polyester or the polyether. Generally speaking, the decomposition temperature for polyurethanes was at about 240 °C, but for hyperbranched polyurethanes, the decomposition temperature was higher than 300 °C22,23.

Table 2. DSC results for HBPUs.

<table>
<thead>
<tr>
<th>Sample</th>
<th>$T_g$ (HPMS-APE) onset, midpoint and endset (°C)</th>
<th>$T_g$ (PPG) onset, midpoint and endset (°C)</th>
<th>$T_m$ (°C)</th>
<th>ΔH (J·g⁻¹)</th>
</tr>
</thead>
<tbody>
<tr>
<td>HBPU0</td>
<td>$-114.1$, $-114.8$, $-101.3$</td>
<td>$-45.7$, $-36.9$, $-22.9$</td>
<td>81.3</td>
<td>9.94</td>
</tr>
<tr>
<td>HBPU1</td>
<td>$-116.6$, $-115.7$, $-102.7$</td>
<td>$-36.2$, $-30.1$, $-18.4$</td>
<td>82.0</td>
<td>3.42</td>
</tr>
<tr>
<td>HBPU2</td>
<td>$-116.3$, $-115.0$, $-102.9$</td>
<td>$-46.3$, $-37.1$, $-24.0$</td>
<td>82.1</td>
<td>6.43</td>
</tr>
<tr>
<td>HBPU3</td>
<td>$-115.2$, $-114.3$, $-101.4$</td>
<td>$-45.3$, $-36.2$, $-23.5$</td>
<td>80.4</td>
<td>6.51</td>
</tr>
<tr>
<td>HBPU4</td>
<td>$-115.2$, $-114.3$, $-101.4$</td>
<td>$-46.5$, $-37.3$, $-24.1$</td>
<td>81.8</td>
<td>6.07</td>
</tr>
</tbody>
</table>

Figure 5. (a) TGA curves of HBPUs, (b) DTG curves of HBPUs.

Table 3. TGA and DTG results for HBPUs.

<table>
<thead>
<tr>
<th>Sample</th>
<th>$T_m$ (°C)</th>
<th>$T_{max1}$ (°C)</th>
<th>$T_{max2}$ (°C)</th>
<th>$W_r$ (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>HBPU0</td>
<td>320.7</td>
<td>344.8</td>
<td>387.3</td>
<td>0</td>
</tr>
<tr>
<td>HBPU1</td>
<td>325.1</td>
<td>343.6</td>
<td>398.4</td>
<td>2.3</td>
</tr>
<tr>
<td>HBPU2</td>
<td>334.2</td>
<td>346.9</td>
<td>406.0</td>
<td>3.6</td>
</tr>
<tr>
<td>HBPU3</td>
<td>332.9</td>
<td>346.9</td>
<td>414.7</td>
<td>4.0</td>
</tr>
<tr>
<td>HBPU4</td>
<td>337.0</td>
<td>348.1</td>
<td>420.1</td>
<td>5.1</td>
</tr>
</tbody>
</table>

From the data, it could be seen that the $T_m$ of HBPUs was about the same up to 320 °C and the $T_{max1}$ of HBPUs changed very little, while the $T_{max2}$ of all HBPUs with HPMS-APE segments were much higher than that of HBPU0 based on pure PPG. The effect of HPMS-APE on the course of degradation was clearly revealed at the second decomposition fraction. The $T_{max1}$ of HBPU0 was the lowest and its value was 387.3 °C. The $T_{max2}$ of HBPU0 increased with the growing content of HPMS-APE, and the incorporation of HPMS-APE increased the $T_{max2}$ as high as 33 °C, which might be ascribed to the greater thermal stability of the HPMS-APE component. In addition, the amount of solid residue after degradation for HBPU4 increased to follow the increasing HPMS-APE content. Those findings seemed to serve as the evidence for the formation of complex PDMS-based structures in the pyrolysis process. Their structures were formed on the surface and probably created the insulating layer which slowed down further decomposition of the polymer, as it was observed for PDMS-based polyurethanes24.

Table 3. TGA and DTG results for HBPUs.

Mechanical tests

To evaluate the effect of HPMS-APE segments content on the mechanical properties of HBPUs, tensile tests and Shore hardness tests were performed, as showed in Figure 6a and 6b, respectively. In all cases, the elongation at break of HBPUs gradually increased with increasing HPMS-APE content because of the flexibility of the PDMS. Hardness scores for HBPUs were within the range of 72 A to 83 A, and there was a tendency for the hardness scores to lower as the HPMS-APE content increased. However, it was noteworthy that the tensile strength remained largely unchanged up to 5 wt% of HPMS-APE, yet increasing HPMS-APE above 10 wt% made HBPUs mechanically weaker than HBPU0 based on pure PPG segments, with HBPU4 showing the lowest tensile strength of the series. Similar observations were reported by Chen21 on the effect of siloxane content on the mechanical properties of PDMS urethanes. The reasons were as follows: the mechanical properties of polyurethanes were profoundly dependent on the degree of microphase separation12, and the enhanced phase mixing between hard and soft segments resulted in the best mechanical properties of HBPU1 with 5 wt% of HPMS-APE, that was in agreement with DSC and AFM analysis. However, when increasing HPMS-APE content above 10 wt%, the tensile strength tended to decrease, resulted from the more HPMS-APE segments content, as well as the excess degree of microphase separation got the negative effect20. Compared with previous work on PDMS-based polyurethane materials, in this study, the incorporation of HPMS-APE in polyurethanes can be controlled to a certain degree, polyurethanes could be prepared without significant compromise in tensile strength and elasticity.

Water absorption testing

As shown in Figure 7, it was found that the water absorption for HBPUs had an obvious decrease with the addition of HPMS-APE, when the content of HPMS-APE increased from 0 wt% to 20 wt%, the water absorption of HBPU0 decreased from 11.28% to 0.73% (72 h). Moreover, with the incorporation of HPMS-APE, the water absorption for HBPUs based on mixed soft segments kept mostly unchanged above 48 h in comparison with HBPU0. In this study, 0-20 wt% of HPMS-APE content was incorporated in polyurethanes, so the degree of microphase separation didn’t influence the water resistance of HBPUs20, and HPMS-APE content appeared to be the sole factor. Due to the strong hydrophobic Si-O-Si bonds and the low surface energy of HPMS-APE segments, polyurethanes had a highly hydrophobic nature, and it brought polyurethanes good hydrolytic stability and fast water release on drying21. Further, the water resistance of these materials was superior to that of previously published PDMS-based polyurethanes22,23. Accordingly, we confirmed that HBPUs derived from HPMS-APE presented excellent water resistance.

CONCLUSIONS

In summary, a series of HBPUs base on HMPS-APE and PPG mixed soft segments were successfully synthesized. The enhanced properties of HBPUs with different content of HMPS-APE segments were characterized by FT-IR, DSC, AFM, TGA, mechanical testing and water absorption. DSC and AFM results confirmed that the incorporation of HMPS-APE as part of the soft segments resulted in enhanced phase mixing between hard and soft segments, and HBPU1 with 5 wt% HMPS-APE appeared to be the most extent of microphase separation between hard and soft segments of the series. Mechanical testing results clearly demonstrated that incorporating 5 wt% HMPS-APE, polyurethanes could be prepared without significant compromise in tensile strength and elasticity.
in tensile strength and elasticity. Furthermore, TGA results indicated that incorporating HMPS-APE in polyurethanes made substantial changes in their thermal stability, increasing $T_{\text{max}}$ as high as 33 °C in comparison with HBPU0 based on pure PPG. Additionally, HBPU0s derived from HPMS-APE presented excellent water resistance, when HPMS-APE increased from 0 wt% to 20 wt%, the water absorption of HBPU0s decreased from 11.28% to 0.73% (72 h).

Figure 7. Water absorption of HBPU0s.

ACKNOWLEDGEMENTS

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