

EXAMINING THE EFFICIENCY OF MECHANIC/ENZYMATIC PRETREATMENTS IN MICRO/NANOFIBRILLATED CELLULOSE PRODUCTION

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ABSTRACT

There is still a need to improve the production sequences of micro fibrillated and nano fibrillated celluloses to obtain more economic and better quality products. The aim of this study was to improve the production efficiency and quality of micro fibrillated and nano fibrillated celluloses by examining the enzyme (xylanase endo-1,4-) employed in pretreatment sequences. Fairly homogeneous nano fibrillated cellulose with a width of 35 ± 12 nm was produced in this study. Sequences employed to produce micro fibrillated and nano fibrillated celluloses decreased the cellulose crystallinity of bleached kraft pulp and lower total crystalline index and lateral order index values were observed for micro fibrillated and nano fibrillated celluloses in FTIR examinations. Lower crystallinities were also defined by ^{13}C -NMR (46,2 ppm) which was substantiated with C6 peaks in the amorphous domain. Sequences to produce micro fibrillated and nano fibrillated celluloses resulted in shorter fiber dimensions with less ordered cellulose structure leading lower thermal degradation that reveal main polymer chain source from cellulose units. Dynamic mechanical thermal analysis results showed that the initial and maximum storage modulus of the nano fibrillated and micro fibrillated celluloses films were improved by 114% and 101%, respectively. The storage modulus of micro fibrillated and nano fibrillated celluloses films were 4,96 GPa and 2,66 GPa at temperature of 235°C, respectively.

Keywords: Biofilm, chemical characterization, Kraft pulp, homogenization, thermomechanical characterization.

INTRODUCTION

Cellulose is one of the most abundant, renewable and biodegradable natural polymers (Habibi *et al.* 2010). It consists of D-glucose subunits which are linked together by -1,4 glycosidic bonds. Intra and inter-molecular bonds in cellulose constructs microfibrils that are packed side by side and generates microfibril bundles. Biopolymers have been progressively processed in nanotech by methods of homogenization, micro fluidization, micro grinding, cryocrushing, acid hydrolysis (Siro and Plackett 2010) and enzyme treatments (Lavoine *et al.* 2012). These processes improve the mechanical and thermal properties of the materials and make them suitable for several industrial applications; papermaking, additives, thickeners, stabilizers, fillers, pharmaceuticals and etc. (Syverud and Stenius 2008, Hettrich *et al.* 2014).

In nanoscale cellulose production, the main component resisting the separation process is lignin. Lignin acts as a protective barrier and obstacles the cell permeability causing insignificant cell destruction. Therefore, lignin removal is necessary for efficient processes (Pérez *et al.* 2002). The other cell wall component, essence of hemicelluloses in the structure also positively affects the production

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efficiency (Agbor *et al.* 2011). On the other hand, physicochemical factors of crystallinity and packed structure affect the production efficiency (Khalil *et al.* 2012). Packed cellulose is insoluble in water as the hydroxyl groups are bonded to each other. In order to improve the production efficiency, the supramolecular structure of cellulose must be disrupted into amorphous phases.

One of the most applied method to produce micro/nano fibrillated cellulose (MFC/NFC) with a high yield is mechanical treatment. However, the method requires vast amount of energy (Spence *et al.* 2011). To overcome the deficiencies of the above explained method, enzymatic pretreatments along with the mechanical treatment applied to reduce the consumed energy (Li *et al.* 2011). For this reason, generally, endoglucanases act to cleave the internal bonds (e.g., noncovalent interaction) present in the amorphous structure of cellulose. Exoglucanases/cellobiohydrolases attack the ends of the cellulose chains which are generated by the endoglucanases. Subsequently, the shorter cellulose chains are further hydrolyzed by cellobiases/beta-glucosidases into nanocellulose or even a glucose product (Lee *et al.* 2014).

In this parallel, Pääkko *et al.* (2007) demonstrated a combination of high shear pressure force and mild enzymatic hydrolysis (monocomponent endoglucanase) by using sulfite pulp to produce MFC by maintaining high aspect ratio with well controlled diameter. In addition, there are number of studies revealing properties of MFC/NFC suspensions and their films (Saito *et al.* 2007, Bismarck *et al.* 2005, Dri *et al.* 2013, Viana *et al.* 2016). Besides, new trend related to MFC/NFC is of their composites with inorganic/organic polymers (Kord *et al.* 2016, Poyraz *et al.* 2017).

There is a gap that explains relations between chemical structure and physical/thermal/mechanical properties in the literature. For that purpose, detailed chemical, rheological and thermal characterization of MFC/NFC suspensions as well as morphology and dynamic mechanical results were studied in this study.

MATERIALS AND METHODS

Materials

For this study, freshly cut logs of a 16-year-old river red gum tree (*Eucalyptus camaldulensis*) brought from Tarsus, Turkey, was used as raw material. The bark and cambium were carefully removed and the logs were reduced to chips suitable for the subsequent kraft pulping operations. The chips were air-dried and screened to establish a uniform size throughout pulping.

The enzyme employed to break down the cellulose and hemicellulose structures was xylanase endo-1,4- (Novozymes, Bagsvaerd, Denmark).

Methods

Pulping and bleaching

Kraft pulp was produced using 500 g of chips (o.d.). The cook was made in a 10 L rotating digester (Uniterm Rotary Digester, Uniterm Lab.) at 150 °C for 150 min after reaching the maximum temperature in 30 min. The calculated H-factor was 410. The cook was achieved at 18% active alkali and 28% sulphidity charges, and the liquor-to-wood ratio (L/kg) was 5:1. The produced pulp was disintegrated and washed with hot tap water, and then screened using a flat laboratory screen (Somerville Flat Screen, Techlab Systems) with a slot width of 0,15 mm (Tappi T275). The pulp yield (screened/unscreened) and rejects were determined according to Tappi T210 via gravimetric measurements in the laboratory environment.

The pulp was bleached using Elemental Chlorine Free (ECF) processes (ODEP: oxygen-chlorine dioxide-alkaline-peroxide). Oxygen (O₂) bleaching was conducted in a digester using 2% NaOH (as Na₂O-o.d. pulp) and 0,5% MgSO₄ (as carbohydrate stabilizer-o.d. pulp) at a pressure of 6 kgf cm⁻² (90 °C for 60 min). The consistency was 10%. The chlorine dioxide (D) bleaching was performed in a

plastic bag placed in a water bath (GFL 1023 Water Bath, GFL Lab.) (60 °C for 60 min) and each pulp (10 g, o.d.) was treated with 100 mL ClO₂ (1%) consisting of 3 mL H₂SO₄ (98%) solution. The alkaline extraction (E) was also performed in a water bath at 60 °C for 60 min and each pulp (10 g, o.d.) was treated with 100 mL NaOH solution (2%). The hydrogen peroxide bleaching (P) was conducted at 10% pulp consistency using 4% H₂O₂, 0,5% Na₂SiO₃ (as hydrogen peroxide stabilizer), 0,1% MgSO₄ and 1,5% NaOH (o.d. pulp). The process was carried out at 105 °C for 120 min in a digester. After each bleaching operation, the pulps were washed with water, squeezed and crumbled.

The kappa number (Tappi T236) and viscosity (degree of polymerization of the cellulose) (SCAN cm 15-62) of the pulps were then determined.

Gel preparation

The cell wall delamination of the bleached kraft pulp was accomplished in four stages: mechanical refining, enzymatic pretreatments, second mechanical refining, and homogenizing. The bleached kraft pulp was first mechanically refined (2% w/w) for 10 min using a Waring blender (NuBlend Commercial Blender, Waring Commercial) to reach 30 °SR (Chang *et al.* 2012). The power input was 1,9 A at 115 V. The process was paused for 5 min to allow the material to cool down to approximately room temperature. The freeness of the pulp was measured using a Schopper Riegler device (SR/P Schopper Riegler, Thwing-Albert Instrument Company) (ISO Standard method 5267-1).

Refined materials (50 g o.d. pulp) were enzymatically hydrolyzed using xylanase endo-1,4- for concentrations of 25, 100 and 250 AXU/g at 2% solid loading in 2,5 L of phosphate buffer at pH 7,0. The phosphate buffer used in the enzymatic pretreatments was prepared from 11 mM KH₂PO₄ and 9 mM Na₂HPO₄. The enzyme reactions were accomplished in an incubator (Incubator ES-20, Biosan Lab.) at 50 °C for 2 h. The samples were mixed manually every 30 min. At the end of the pretreatment, the samples were washed with deionized water and put into boiling water for 30 min to stop the enzymatic activity. Then the samples were again washed with deionized water. The highest ratio of removed glucan to xylan was obtained with enzyme concentration of 100 AXU/g (0,84: 25 AXU/g; 0,99: 100 AXU/g; 0,77: 250 AXU/g). For that purpose the sample with the highest amount of xylan was selected for further analysis.

The enzymatically pretreated sample was then refined again using a Waring blender (NuBlend Commercial Blender, Waring Commercial) (Chang *et al.* 2012), to reach 90 °SR. To prevent a bacterial growth in the material 0,4 µL/mL of a microbicide (5-chloro-2-methyl-4-isothiazolin-3-one) was added to the slurry.

In the MFC and NFC production stage, the sample was passed through a high-pressure fluidizer (2% w/w) (Microfluidizer M-110Y, Microfluidics Corp.). For the MFC production, the sample was passed one time through a Z-shaped chamber with a diameter of 200 µm (14000 psi). For the NFC production, the sample was passed once through a Z-shaped chamber with a diameter of 200 µm (14000 psi) and then passed five times through a chamber with a diameter of 100 µm (24000 psi).

Film manufacturing procedure

For MFC or NFC film manufacturing, the MFC or NFC was stirred for 1 h at room temperature to ensure homogeneous consistency. The MFC or NFC suspension was poured onto a glass plate. The materials were placed in a dryer to evaporate water at 60°C for overnight. The NFC or MFC films were peeled off from the plate and kept at room temperature for 24 hours before the dynamic mechanical thermal analysis (DMTA).

Analytical methods

HPLC (High-performance liquid chromatography) Analysis: The sugar and the lignin contents of the samples were determined by Laboratory Analytical Procedures (LAP) from the National Renewable Energy Laboratory (NREL) (Sluiter *et al.* 2004). The sugar contents were analyzed using the HPLC (Agilent 1200 System, Agilent Tech.) equipped with a Shodex SP0810 column (mobile phase: HPLC

grade water-0,2 μm filtered and degassed; injection volume: 20 μL ; flow rate: 0,6 ml/min; column temperature: 80 $^{\circ}\text{C}$) and a refractive index detector. The acid-insoluble and acid-soluble lignin were determined, respectively, by weighing and by the adsorption at 320 nm against a deionized water blank.

The reduction in lignin was calculated based on the initial dry weight of the lignin in the both chip and bleached kraft pulp (LU) and the dry weight of the lignin in the remaining solids after the pulping, bleaching, refining, enzymatic hydrolysis and homogenizing treatments (LP). The percentage of lignin reduction was calculated with the following Equation 1:

$$\text{The percentage of lignin reduction} = \frac{LU - LP}{LU} \times 100 \quad (1)$$

The solubilization of xylan and glucan during the treatments was also calculated in the same manner.

Furthermore, the percentage of solids recovered was calculated on an oven-dry basis as follow Equation 2:

$$\text{The percentage of solids recovered} = \frac{W2}{W1} \times 100 \quad (2)$$

where W1 is the dry weight of the whole biomass before treatment (g), and W2 is the dry weight of the treated material (g).

FTIR (Fourier transform infrared) Spectroscopy: The IR spectra were taken via an attenuated total reflectance (ATR)-FTIR device (Shimadzu IR Prestige-21, Shimadzu Corp.). Sample suspensions of 0,5 ml were prepared in a concentration of 2% (w/w). The samples were gently dropped in a diamond attachment using an automatic pipette (0,1-1 ml). In order to elucidate molecular vibration signals in the range of 4000-600 cm^{-1} , 20 scans with a resolution of 4 cm^{-1} were taken.

¹³C CP/MAS NMR (Cross Polarization Magic Angle Spinning Nuclear Magnetic Resonance) Spectroscopy:

The solid state ¹³C CP/MAS NMR spectra of the samples were recorded using an Advance III 300-MHz NMR instrument (Bruker Corp.). The operating frequency was fixed at 75385 MHz. A double air-bearing probe and a zirconium oxide rotor (4 mm) were used in the analysis. The MAS rate was 8500 Hz. A CP pulse was ramped at a contact pulse of 100 μs with the rotation of 4 μs proton at 90 $^{\circ}$ pulse (294,8 $^{\circ}\text{K}$). The delay between repetitions was 2,5 s.

Rheological Measurements

In order to determine the rheological properties of the samples, a RST-CPS Rheometer (Brookfield Corp.) was used. The measurements were made at the 37,5 mm diameter cone-plate and the 25 mm diameter parallel plate. The gap was fixed at 1 mm. Before the measurements, the shearing was applied to the materials at 20000 rpm for 2 min (IKA T18 homogenizer, IKA Lab.) to disrupt any flocculated aggregates and the samples were then allowed to rest for 3 min.

SEM (Scanning Electron Microscopy)

The morphological properties of the samples were analyzed by taking SEM (FEI Quanta FEG 250, FEI Corp.) images. The samples were first dried at 105 $^{\circ}\text{C}$ overnight, and then coated up to 5 nm with a gold-palladium composite. Pictures were taken for all samples at 1-15 kV using a field emission gun equipped with a compacted secondary electron detector. Scales were selected as 100 μm for fiber materials and 1 and 100 μm for MFC and NFC. In addition, SEM analyses were carried out for MFC or NFC films.

Thermal Analysis

The thermal properties of the materials were examined using thermogravimetric analysis (TGA). For the TGA, a Shimadzu DTG 60 (Shimadzu Corp.) equipped with a thermal analysis data station was utilized. The material samples were first dried at room temperature overnight. Approximately 5 mg of the material was placed in a platinum pan and heated from room temperature to 650 °C at a rate of 20 °C/min. Measurements were carried out under nitrogen flow (75 mL min⁻¹). The mass of the material was recorded as a function of the temperature.

Dynamic Mechanical Thermal Analysis (DMTA) of Nanofilms and Microfilms

DMTA tests were carried out to obtain thermo-mechanical characteristics (storage modulus) of the produced MFC and NFC films. The test was performed in tension mode at a controlled heating rate of 5°C/min. The temperature raised from 30 °C to 250 °C at an oscillatory frequency of 1 Hz.

RESULTS

Yield, kappa and viscosity (degree of polymerization of the cellulose) analyses

The screened yield of kraft pulp for the eucalyptus was 45,6% (o.d. chip) and a very small amount of the reject obtained (0,03% o.d. pulp). The kappa number and viscosity were 18,4 and 10,2 cP respectively (Table 1). Bleaching sequences diminished the kappa number and viscosity and the decrease of kappa number and viscosity for the final bleached pulp were 83,6% and 47,1% respectively.

Table 1. Yield, kappa and viscosity values of kraft pulp after each bleaching stage.

Bleaching stages	Total Yield, %	Kappa	Viscosity, cP
Kraft	45,7 ± 0,46	18,4 ± 0,15	10,2 ± 0,38
Kraft-O	44,8 ± 0,17	10,4 ± 0,00	9,50 ± 0,26
Kraft-O-D	44,7 ± 0,22	4,16 ± 0,00	5,15 ± 0,21
Kraft-O-D-E	41,9 ± 0,34	3,59 ± 0,09	5,60 ± 0,10
Kraft-O-D-E-P	41,5 ± 0,26	3,02 ± 0,01	5,40 ± 0,10

Chemical properties

HPLC analyses

The chemical composition of wood and un/bleached pulps were given in Table 2. The HPLC analyses showed that the total carbohydrate of *E. camaldulensis* was 49,3% (o.d. chip). Glucan, the major cell wall component, made up 40,0% (o.d. chip), and xylan, the major hemicellulose constituent, was 8,67% (o.d. chip). Mannan, arabinan and galactan accounted for only 0,62% (o.d. chip). The total lignin (acid insoluble/soluble) was 28,3% (o.d. chip) (Table 2). The glucan contents of un/bleached kraft pulps were 61,8 and 66,3% and the xylan contents of un/bleached kraft pulps were 15,3 and 14,3% (w/w), respectively.

Table 2. Chemical composition of pulps after pulping and bleaching.

Chemical Components (%)			
	Chips	Unbleached Kraft	Kraft (ODEP)
Glucan	40,0 ± 1,53	61,8 ± 2,04	66,3 ± 0,90
Xylan	8,67 ± 0,19	15,3 ± 0,65	14,3 ± 0,85
Galactan	0,18 ± 0,14	-	-
Mannan+Arabinan	0,44 ± 0,20	0,33 ± 0,00	0,67 ± 0,00
Acid Insoluble Lignin (AIL)	27,6 ± 0,99	1,98 ± 0,54	0,40 ± 0,09
Acid Soluble Lignin (ASL)	0,74 ± 0,01	1,05 ± 0,02	1,16 ± 0,41
% removed material (o.d. chip)			
Total material	-	54,4	58,5
Glucan	-	29,5	31,2
Xylan	-	19,5	31,6
Total lignin	-	95,1	97,7

Alterations in chemical compositions of bleached kraft pulp after mechanical and enzymatical pretreatments and then homogenization were shown in Table 3. Mechanical pretreatment diminished the glucan (1,80% o.d. bleached pulp) and xylan (0,20% o.d. bleached pulp) contents. Varying enzyme concentrations applied in this study resulted in 65% (25 AXU/g) to 66,8% (100 AXU/g) (w/w) of glucan and 13,8% (250 AXU/g) to 14,4% (100 AXU/g) (w/w) of xylan contents. The studied enzyme concentration for further process was determined regarding the removal of glucan to xylan ratio. The determined concentration for further process was 100 AXU/g. This sample was mechanically pretreated again and the obtained sample had 66,3% of glucan and 14% xylan (w/w) in the structure. The samples were then homogenized and MFC and NFC were produced. Results showed that MFC and NFC had 66,3 and 65,9% (w/w) of glucan and 13,9 and 13,8% (w/w) of xylan in the structure, respectively.

Table 3. Changes in chemical components of kraft pulp after mechanic/enzymatic pretreatments and homogenization.

Chemical Components (%)	First refining	Enzymatic treatment (Concentrations, AXU/g)			The enzyme treated sample (Concentration of 100 AXU/g)		
		25	100	250	Second Refining	MFC	NFC
Glucan	65,7 ± 0,07	65,0 ± 0,02	66,8 ± 0,91	65,8 ± 0,08	66,3 ± 0,56	66,3 ± 0,05	65,9 ± 0,01
Xylan	14,5 ± 0,24	13,9 ± 0,12	14,4 ± 0,04	13,8 ± 0,11	14,0 ± 0,10	13,9 ± 0,19	13,8 ± 0,82
% removed material (o.d. chip)							
Glucan	33,0	34,2	34,9	35,8	35,9	35,9	36,2
Xylan	31,8	35,1	35,2	37,5	37,5	38,0	38,4
% removed material (o.d. bleached kraft pulp)							
Glucan	2,56	4,32	5,32	6,73	6,75	6,75	7,31
Xylan	0,31	5,14	5,37	8,65	8,70	9,36	10,0

FTIR analyses

The molecular interactions of bleached kraft pulp, MFC and NFC produced in this study were investigated by FTIR (Figure 1). In the spectra, the slightly broad O-H stretching peaks observed at 3328 cm⁻¹ matched to the free OH groups of the cellulose molecules corresponding to intra and intermolecular H-bonds. O-H in-plane bending vibration was additionally observed at 1336 cm⁻¹.

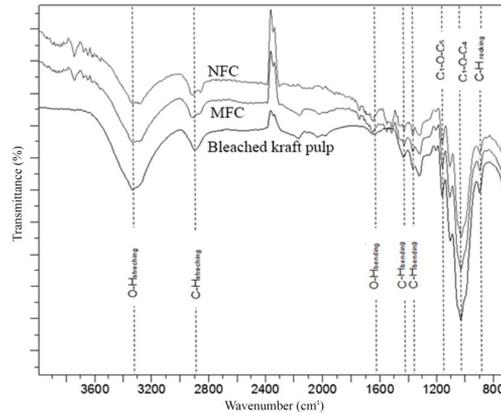


Figure 1. FT-IR spectras for bleached kraft pulp, MFC and NFC.

Lignin peaks, 1740 cm^{-1} (carbonyl), 1509 cm^{-1} (aromatic C=C ring deformation) and 1463 cm^{-1} (C-H deformation), were not observed in this study. Peaks at about 1163 cm^{-1} are related to $C_1\text{-O-C}_5$ asymmetric bridge stretching and the peaks reveal the ether linkage in the pyronose rings. In addition, the peak intensity of the glycosidic deformation or pyranose ring skeletal stretching was observed at 1033 cm^{-1} ($C_1\text{-O-C}_4$).

The total crystalline index (TCI) (A_{1378}/A_{2900}) of the samples were calculated regarding the ratio between CH_2 asymmetric stretching vibration peaks (2900 cm^{-1}) and C-H asymmetric deformation vibration (1378 cm^{-1}). In addition, Lateral Order Index (LOI) (A_{1437}/A_{899}) value indicating the β -glycosidic linkages between glucose units was calculated regarding the intensity ratio between in-plane scissoring (symmetric bending) (1437 cm^{-1}) and C-H rocking (897 cm^{-1}). The calculated values of TCI and LOI were shown in Table 4.

Table 4. Total crsyalline ratio and lateral order index obtained from the FT-IR analysis of cellulose samples studied.

	TCI ($1378\text{ cm}^{-1}/2900\text{ cm}^{-1}$)	LOI ($1437\text{ cm}^{-1}/899\text{ cm}^{-1}$)
Bleached Kraft Pulp	$0,488 \pm 0,011$	$1,638 \pm 0,021$
MFC	$0,462 \pm 0,008$	$1,592 \pm 0,018$
NFC	$0,441 \pm 0,007$	$1,571 \pm 0,012$

^{13}C -NMR analyses

The chemical structures of the samples were analyzed by CP/MAS ^{13}C -NMR (Figure 2). Results showed that the intensity of the peaks decreased from bleached kraft pulp to MFC and then to NFC.

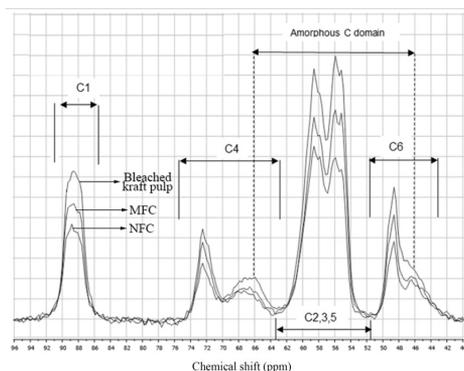


Figure 2. ^{13}C -NMR spectra for bleached kraft pulp, MFC and NFC.

The spectroscopy used to distinguish between crystalline (ordered) and amorphous (less-ordered) cellulose based on the chemical shifts and clusters in C4 and C6 peaks. Sharp signals imply well ordered (crystalline) regions whereas broad signals show less ordered regions (amorphous). The left domains of both C4 and C6 peaks displayed the crystalline character whereas the right domains of both showed the amorphous character (Figure 2). The most intense peaks were related to C2, C3 and C5 positions, which were observed at around 61-53 ppm.

Rheological properties

The rheological properties of bio-based suspensions are of vital importance for the prediction of composites performance for the potential end applications. The viscosity was plotted as a function of the shear rate for bleached kraft pulp, MFC and NFC samples (Figure 3). The produced NFC had the lowest viscosity.

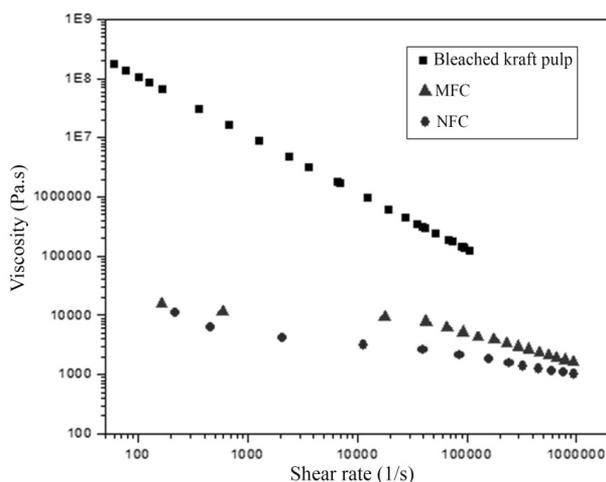


Figure 3. Viscosity as a function of the shear rate for bleached kraft pulp and MFC-NFC materials.

Morphological (Structural) properties

Figure 4 shows the SEM images of bleached kraft pulp (Figure 4a), MFC (Figure 4b) and NFC (Figure 4c) samples. The fiber width of the bleached pulp was in micron size. The SEM images of MFC and NFC was pictured at two different scales (100 μm and 1 μm). MFC samples pictured at the 100 μm scale showed some micron-wide fibers. On the other hand, some nanofibrils were apparent in images taken at 1 μm . The NFC sample examined at the 100 μm scale had none micron width fibers. These

indicated that the method utilized in this study resulted in fairly homogeneous NFC production. The generated nanofibers had a rod-like structure with an average length (3820 ± 170 nm) and width (35 ± 12 nm). The average aspect ratio of NFC was 115 ± 35 .

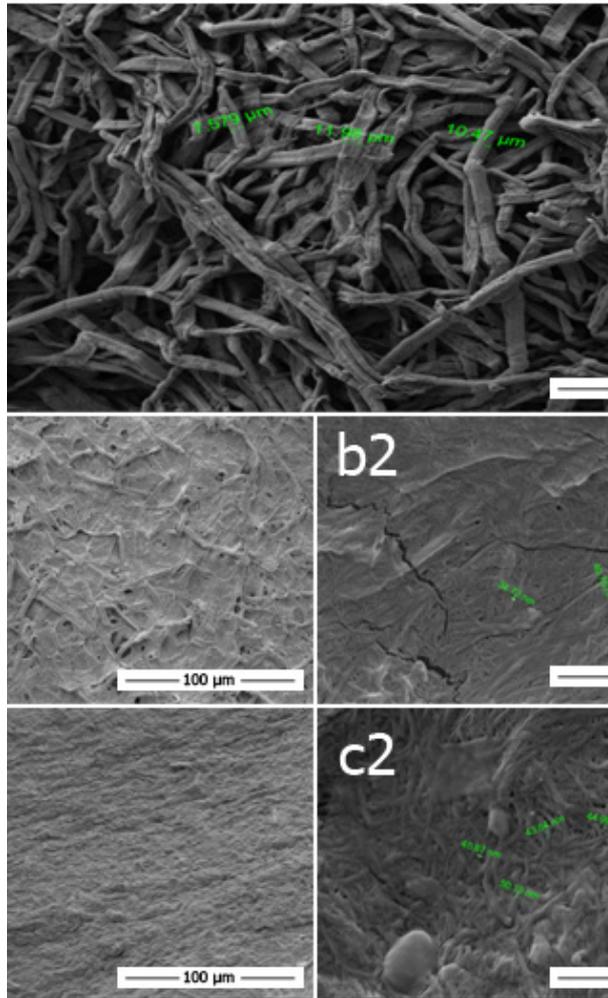


Figure 4. SEM images: (a) bleached kraft pulp, (b1-2) MFC and (c1-2) NFC materials.

Thermal analysis

The TGA curves of the bleached kraft pulp, MFC and NFC were given in Figure 5. All analyzed samples were exposed to two-step degradation processes. Initial weight losses started at 25°C and then preceded up to 180°C . Bleached kraft pulp lost the highest moisture compared to NFC and MFC.

A significant weight loss was observed at about 320°C - 400°C . The NFC showed the lowest thermal decomposition and thermal stability (318°C) as well as broader degradation range compared to bleached kraft pulp (340°C) and MFC (328°C).

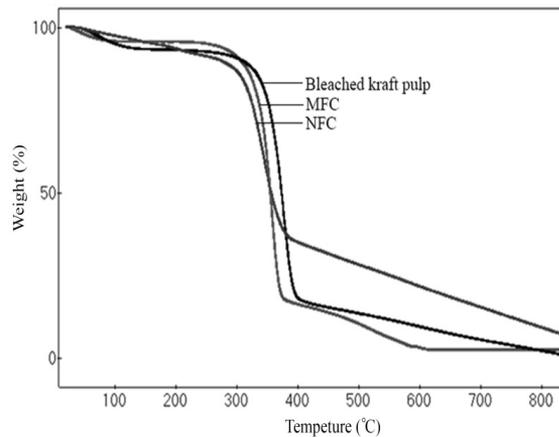


Figure 5. TGA thermograms for bleached kraft pulp, MFC and NFC.

Dynamic mechanical thermal analysis (DMTA) of nano/micro films

The films of MFC and NFC were shown in Figure 6. DMTA showed that the storage modulus values of the NFC and MFC films increased with increasing temperature from 30 °C to 84 °C and 30 °C to 104 °C, respectively. After reaching the maximum point, the storage modulus values of the NFC and MFC films decreased with increasing the temperature up to 230 °C.

Figure 6 showed that the storage modulus of the NFC and MFC films for the temperature of 30°C were observed to be 6,04 GPa and 2,82 GPa respectively. The maximum storage modulus values for NFC and MFC were 7,68 GPa and 3,82 GPa respectively.

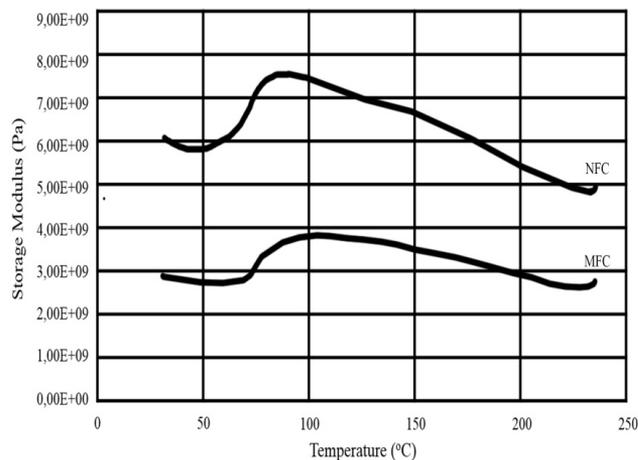


Figure 6. Storage modulus results of the nano- or micro films.

DISCUSSIONS

Yield, kappa and viscosity (degree of polymerization of the cellulose) analyses

The yield, kappa and viscosity values of un/bleached kraft pulp are shown in Table 1. Ayata (2008)

utilized the same wood species and pulping conditions, found similar yield, kappa and viscosity for the unbleached kraft pulp. Bleaching removed the lignin from the structure and it was noted that the kappa number and viscosity values decreased when the pulp was bleached in this study. A significant decrease in viscosity and kappa was observed when pulp was bleached with chlorine dioxide. This finding could be explained by lignin delignification and polysaccharide degradation during bleaching stage (Barroca *et al.* 2001). The NaOH (E) used in the bleaching stage in addition extracted some lignin as well as low molecular weight carbohydrates and consequently diminished the total yield. On the other hand, a slight increase in pulp viscosity during E stage bleaching (5,60 cP) was observed in this study. Similar finding was observed earlier by Islam (2004). This finding could be explained by the removal of some low molecular weight materials from the structure.

Chemical properties

HPLC analyses

The chemical composition of wood and un/bleached pulps were shown in Table 2. The chemical compositions of wood determined in this study were comparable with the findings of Moussaouiti *et al.* (2012). The lignin, glucan and xylan solubilizations were found to be 97,7%; 31,2% and 31,6% (o.d. chip) for the bleached pulp, respectively. The proportional increase in glucan content for both un/bleached kraft pulps was explained by the lignin delignification. The kraft pulp had 15,3% xylan and bleaching slightly decreased the xylan content. Removal of xylan with lignin could be due to the lignin carbohydrate complexes (LCC).

The bleached kraft pulp was first mechanically pretreated and the treated samples had slightly lower glucan and xylan contents. Chen *et al.* (2013) also observed similar results. It was shown that the enzyme had minor effect on glucan degradation (Table 3). The enzyme preserved the xylan in the structure diminished the cell wall cohesion and resulted in easier cell wall delamination (Kolakovic 2013). This in addition prevented the blocking in the homogenizer (Pääkko *et al.* 2007). Consequently, the enzyme concentration (100 AXU/g) applied in this study removed up to 5,37% (o.d. bleached kraft pulp) of the xylan. The sample was then mechanically pretreated and the results showed almost no xylan or glucan degradation. On the other hand, when MFC and NFC were produced the samples had slightly lower amount of xylan and glucan (Virtanen *et al.* 2014, Zhang 2013).

FTIR analyses

O-H stretching peaks observed at 3328 cm^{-1} indicated the successive pretreatments of MFC and NFC production which led gradual decrease in O-H peak intensity when compared to bleached kraft pulp (Mandal and Chakrabarty 2011, Ang *et al.* 2012, Poletto *et al.* 2014). This finding implied that pretreatments to produce MFC and NFC caused insignificant cellulose disintegration as well more specific surface area in the samples (Abraham *et al.* 2013, Ng *et al.* 2015, Popescu *et al.* 2011, Jiang and Hsieh 2013). The progressively decreasing peaks observed at 1336 cm^{-1} had the similar reaction pattern alike O-H stretching peaks (Jonoobi *et al.* 2009). Lignin content in this study have not been detected at 1740 cm^{-1} , 1509 cm^{-1} and 1463 cm^{-1} vibrations (Abraham *et al.* 2013, Mandal and Chakrabarty 2011). It was seen that these vibrations remained limit of detection after FTIR analysis due to the fact that suspensions having minor lignin moieties. The peak intensity observed at 1033 cm^{-1} ($\text{C}_1\text{-O-C}_4$) decreased and this finding showed the degradation of the cellulose chains during the MFC and NFC production (Proniewicz *et al.* 2001, Oh *et al.* 2005).

TCI is closely related to the crystallinity and the degree of the intermolecular bonds (Carrilo *et al.* 2004, Poletto *et al.* 2014). LOI has been used as an evidence for the presence of cellulose I in the cellulosic materials (Ang *et al.* 2012, Mandal and Chakrabarty 2011). Besides, cellulose II formation was observed in amorph structure after pretreatments (Oh *et al.* 2005). LOI and TCI were correlated with the overall degree of cellulose order (Poletto *et al.* 2014, Oh *et al.* 2005). Results showed that bleached kraft pulp had the highest TCI and LOI values revealing the highest crystallinity compared to MFC and NFC. On the other hand, MFC and NFC with lower cellulose infrared crystallinity indicated a larger number of amorphous domains in their structure. This finding was also supported with $^{13}\text{C-NMR}$ (46,2 ppm), which was substantiated with C6 peaks in the amorphous domain. The disorder

of cellulosic structure may be due to the deformation vibration of β -glycosidic linkages and hydrogen bond rearrangements.

¹³C-NMR analyses

The chemical shifts were generally observed in the range of 110-60 ppm (Newman 2004, Park *et al.* 2009). In this study, chemical shifts were observed at 90-45 ppm. This is attributed to the packing effect of the supramolecular structures stemming from chemical reactions, physical processes, etc. (Zuckerstätter *et al.* 2009).

The intensity of the peaks was highest for the bleached kraft pulp compared to MFC and NFC. Results showed that pretreatments to produce MFC and NFC caused some structural deformations in glucose units (Duchesne *et al.* 2001, Newman 2004).

Crystalline and amorphous domains were observed as separate doubled-collateral peaks at 63-76 ppm and 45-51 ppm (Maheswari *et al.* 2012, Park *et al.* 2009). Exception was only observed in C6 for the bleached kraft pulp. These indicated the alterations in samples crystallinity which was also verified by TCI and LOI values.

C2, C3 and C5 peaks were observed at around 61-53 ppm. Results showed that pretreatments had no significant effect and the peaks of bleached kraft pulp, MFC and NFC were almost identical.

Rheological properties

The viscosity of the suspensions decreased with the increase in the shear rate. This might be due to the shear thinning behavior of the suspensions. Because, at the beginning, MFC and NFC suspensions had a tendency to become unstable due to flocculation and entangled thicker fibers in the network. Later, this flocculation and entanglement started to disappear with applied shear rate. Therefore, shear thinning behavior was observed in the suspensions. Consequently, the suspensions are evaluated as pseudoplastic materials in this study. The suspensions were viscous under normal conditions, but the viscosity of the suspensions was decreased when the suspension was stressed and the shearing forces were removed (Berca and Navard 2000, Pääkko *et al.* 2007).

To obtain MFC and NFC, processes of enzymatic and mechanical pretreatments followed by homogenization significantly diminished the viscosity of the suspensions. This decrease could be explained by the lower floc size, higher narrow size distribution, gradual breaking of 3D network as well as Einstein coefficient: higher length to diameter ratio (Dufresne 2012, Jia *et al.* 2014).

Morphological (Structural) properties

SEM images of the bleached kraft pulp, MFC and NFC was shown in Figure 4. Mechanical refining swells the fibers and creates damaged zones, which enhances the enzymatic activity (Pääkko *et al.* 2007). Enzymatic pretreatments improve the fibrillation and results in efficient homogenization.

Trials to produce MFC and NFC from mechanically refined pulp (without enzymatic pretreatment) caused blockage in the constriction chambers of the homogenizer. SEM images for these samples showed a large fraction of intact fibers in the structure. Applying only mechanical shearing causes less fiber swelling which damages fibrillar structure. In addition, the process required excessive energy and was therefore not feasible to produce well-defined nanoscale cellulose elements. On the other hand, strong acid hydrolysis is an aggressive process and yields low aspect ratio cellulose elements (Pääkko *et al.* 2007). Consequently, less aggressive enzymatic hydrolysis (xylanase endo-1,4-) was applied in this study. According to the HPLC results, the highest xylose-containing pulp (concentration of 100 AXU/g) was selected as the optimum for xylanase endo-1,4- pretreatment, and thus resulted in easier MFC and NFC production. Easier production could be explained by higher hemicellulose content of the sample which decreased the cell wall cohesion and made cell wall delamination easier (Kolakovic 2013, Pääkko *et al.* 2007).

When enzymatically hydrolyzed pulps were mechanically refined, the efficiency of homogenization was improved and intense cell wall delamination was observed. The pass of the material once through the 200 μm chamber (14000 psi) was certainly enough to produce MFC. This finding could be due to the samples having higher hemicellulose content causing better fiber swelling.

Fairly homogeneous NFC was produced in this study and cellulosic nanofibers had an average length of 3820 ± 170 nm and a width of 35 ± 12 nm. NFC was generated with the average aspect ratio of 115 ± 35 . Moon *et al.* (2011) produced NFC with almost similar method to this study having a diameter of 4 to 10 nm and length of several micrometers with the aspect ratio (>100). Zimmermann *et al.* (2010) obtained nanofibrils from mechanically pretreated sulfite pulp after passing material from the microfluidizer. The width of the nanofibrils was less than 100 nm and they had a high length ratio. On the other hand, super-grinding produced nanofibrils having a width of 20-90 nm (Taniguchi and Okamura 1998). It was concluded that fibers can be degraded to nanoscale by exposing them to shearing stresses in the longitudinal fiber axis. It seems that microfluidizers and super-grinders have a similar effect and nanofibrils of a similar size were produced with microfluidizers in this study. In the case of using sulfite pulp, when the fibers were mechanically and enzymatically pretreated, Ankerfors *et al.* (2009) obtained nanofibrils with a width of 10-20 nm using microfluidizers. The lower size could be due to the pulp type having a higher hemicellulose content, as compared to the kraft pulp utilized in this study. Leitner *et al.* (2007) used an APV Gaulin laboratory-type homogenizator (10-15 pass at 300 bars) and produced 30-100 nm-width nanofibers from mechanically pretreated sugar cane pulp processed with chemical methods.

Thermal analysis

The first degradation could be attributed to losses of the moisture and low molecular weight compounds. Water was found as chemisorbed, loosely bound and free. The bound water in the structure is also observed in FTIR spectra (1650 cm^{-1}) (Mandal and Chakrabarty 2011). Of the samples, bleached kraft pulp had the highest moisture content.

A significant weight loss observed at about 320-400 $^{\circ}\text{C}$ could be due to the cellulose and hemicellulose decomposition (Luduena *et al.* 2011). Also this mass loss revealed that cellulose polymer degradation (Zoppi and Gonçalves 2002).

The highest degradation temperature of 338 $^{\circ}\text{C}$ was needed for the most crystalline bleached kraft pulp (Kim *et al.* 2010). The calculated TCI and LOI values and ^{13}C -NMR results of C6 peaks also supported the thermal stability observations in this study. Pretreatments to produce MFC and NFC caused less ordered and packed cellulose regions as well as shorter fiber dimensions that resulted in lower thermal degradation (Jiang and Hsieh 2013, Shimazaki *et al.* 2007). Up to 650 $^{\circ}\text{C}$, additional decomposition of hemicellulose and lignin was observed (Yang *et al.* 2007). The highest solid residue was observed for the NFC and the result may be due to the presence of more stable cellulose I in the sample (Mandal and Chakrabarty 2011, Spiridon *et al.* 2010).

Dynamic mechanical thermal analysis (DMTA) of nano/micro films

The initial and maximum storage modulus values of the NFC and MFC films were improved by 114% and 101%, respectively. The storage modulus values of the films were 4,96 GPa and 2,66 GPa at temperature of 235 $^{\circ}\text{C}$, respectively. The storage modulus of the NFC film was enhanced by 86% at high temperatures. The results clearly showed that overall performance or high temperature performance of the NFC was higher when compared to MFC. Composite materials having NFC have higher mechanical performance than composite materials having MFC (Arjmandi *et al.* 2015). Similar findings were obtained by Honorato *et al.* (2015) who determined the storage modulus (7,20 GPa) of the TEMPO-oxidized NFC films. Bulota (2012), who developed TEMPO-oxidized NFC films concluded that increase in the storage modulus of the samples were observed when NFC content was increased.

CONCLUSIONS

Biopolymers are of significant application for industry. In this study, fairly homogeneous NFC gel (3820 nm/35 nm/115; length/width/aspect ratio) was prepared. The enzyme xylanase endo-1,4-effectively degraded the glucan and xylan in the structure of the kraft pulp as well as improving the fibrillation. This circumstance paved the way efficient homogenization. Molecular structure of the MFC and NFC exhibited minor differences compared to kraft pulp and also different crystallinity was observed in the samples. Lower crystallinity value was observed in the NFC. Shear thinning behavior was observed in all samples, while the NFC had the lowest viscosity value. NFC and MFC films were successfully fabricated as well. Storage moduli of the MFC and NFC films revealed similar trend and the NFC film gave the highest thermomechanical properties over the room temperature.

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