

# EVALUATION OF PALM FIBER COMPONENTS AN ALTERNATIVE BIOMASS WASTES FOR MEDIUM DENSITY FIBERBOARD MANUFACTURING

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## ABSTRACT

This work deals with assessing the date Palm component wastes as alternative lignocellulosic material for production of Medium density fiberboards, in order to establish economic and balance between production/consumer ratio at different provinces rather than Upper Egypt. Palm leaf and Palm frond was used as Medium density fiberboards precursors. Different urea formaldehyde levels (10-14%/fiber) and pressing pressure (2.5-3.5 MPa) were applied in this evaluation. The acceptable interaction of Palm fibers component with urea formaldehyde was optimized by characterizing its differential scanning calorimetry and thermogravimetric analysis, in comparison with commercial used sugarcane bagasse fibers. The promising Medium density fiberboards Panel is obtained from Palm frond fibers and its mechanical and water resistance properties fulfill the ANSI standard for high grade Medium density fiberboards wood products, especially on applying urea formaldehyde level 12-14%, and pressing pressure 3,5 MPa. It is interesting to note that, applying higher pressing pressure together with 12% urea formaldehyde level provided Palm frond-based Medium density fiberboards with static bending properties, higher than commercial bagasse-based Medium density fiberboards. The insignificant effect of pressing pressure was noticed on water swelling property and free-HCHO of Medium density fiberboards panels. Where, both type of fibers have the same water swelling property (reached ~ 10%), and free-HCHO (~ 27 mg/100g board).

**Keywords:** Date Palm components, defibration process, fibers interaction, strength properties, thermal behaviour, urea formaldehyde, water resistance property.

## INTRODUCTION

In Egypt agricultural wastes accumulate in huge quantities, it reaches about 35 MT/year. Part of this amount is used as animal fodder and to produce energy; as well as in production of paper and engineered wood products (particle and fiber boards). Still large amount of agro- wastes remains unused and it is burned in the open atmosphere causing environmental pollution. In laboratory scale some of wastes were used as filler for rubber composites, carbon materials, and hydrogels for water purification (El-Nashar *et al.* 2004, Ayrilmis and Winandy 2009, Basta *et al.* 2009, Basta *et al.* 2011, Sivakumar *et al.* 2012, Basta *et al.* 2013, Basta *et al.* 2014a and Basta *et al.* 2014b, Fathy *et al.* 2017). Sugar-cane bagasse (SCB) regards the main residue available and used as precursor for production of engineered wood products (particle-boards and Medium density fiberboards; MDF) and paper, in Upper Egypt. Our previous work was focused on examining the ability of controlling the steam digestion step; to improve the strength of SCB-based MDF produced (Adam *et al.* 2012). Medium density fiberboards (MDF) and particleboards have replaced the natural wood, and plywood in

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many furniture applications. MDF is superior to particleboards due to its properties including strength, homogeneity and machining performance (Akhtar *et al.* 2008, Halvarsson *et al.* 2008). They are also appropriate for interior and exterior construction, as well as in industrial applications. The preparation of particleboards and MDF in mill scale started from about four decades. The possibilities of utilizing the available agricultural wastes, (e.g., wheat, bagasse, rice straws, peanut husks, and hazelnut shells), using urea-formaldehyde, melamine-modified urea-formaldehyde, and soy-bean-pMDI adhesive systems in the production of engineered wood products has sparked attention with many authors (El-Saied *et al.* 1996, Faraji 1998, Lee *et al.* 2006, Ye *et al.* 2007, Akgul and Toslughu 2008, Copur *et al.* 2008, Hossein 2009, Ciannamea *et al.* 2010, Abolfazl and Ahmed 2011, Li *et al.* 2011, Basta *et al.* 2011, Basta *et al.* 2014a, Basta *et al.* 2014b and Basta *et al.* 2016, Younesi-Kordkheili and Pizzi 2018). Other trials in producing green artificial wood were carried out by using HCHO-free adhesive and changing the surface properties of natural lignocellulosic fibres by different grafting techniques (Roffael *et al.* 2011, Thakur *et al.* 2012a, Thakur *et al.* 2012b, Thakur *et al.* 2012c, Thakur *et al.* 2014), or by in-situ grafting of agro-fibres with the free styrene containing polyester (El-Saied *et al.* 2012). To improve the water resistance (WA and TS) of wood fibers-based MDF together with limitation of formaldehyde emission of promotion of the quality of the resins, wollastonite and its nano-particles were used in internal and surface treatments (Taghiyari and Nouri 2015, Taghiyari and Nouri 2016). However, surface treatment of MDF by Calcite (100%), clay (100%) or mixture of clay/calcite did not cause a significant difference on surface quality (Istek *et al.* 2012).

Date Palm is a multi-purpose tree; it regards a highly national heritage in many countries. It provides food, shelter, timber products. Because of these qualities, and its tolerance to harsh environmental desert conditions, areas under cultivation have increased tremendously in last decades (Mahmoudi *et al.* 2008). Egypt is the largest date producing country in the world. In 2012, it produced 1,47 million tones that make 19% of world dates production. Cultivation of date Palms in Egypt dates backs to thousands of years. Approximately seven million fruiting Palm trees are grown in Egypt in the Nile Valley, Sinai and similar areas.

Based on the availability of Palm date, as well as the environmental and economical impacts of sugar-cane bagasse from storage processes, the objective of this study is focused on evaluating the interaction of Palm component wastes (date Palm pruning mixed products, leaves & frond), with commercial UF to be alternative substrate to manufacture of MDF. The success of this alternative material will be supported by comparing the MDF properties resulted from promising Palm component with that produced from bagasse fiber and the standard specifications (ANSI 208.2).

## MATERIALS AND METHODS

### MDF Fibers and board preparation

Date Palm rachises (DPR) were collected from date Palm trees grown up at Sinai. The used species is "EL BARMATODA". DPR were air dried in sun light for 48 hours, and then cut to 25x25x3 mm chips. These chips were softened by steam in a horizontal digester. The steam pressure was maintained at ~ 0.8 MPa for 6 min. then defibrated through ANDRITZ refiner parallel experiments, sugarcane bagasse (SCB) samples were also subjected to the same condition of digestion and refining. The softening fibers were sunlight dried and mixed through laboratory blender with different levels of urea formaldehyde (UF) adhesive (based on oven dry basis) ratios as shown in Table 1. The UF was delivered from Speria Co., with free-formaldehyde (HCHO) 0,18 %. The ammonium sulfate (1%based on UF) was added as hardener, followed by 1 % paraffin wax (based on dry fibers). The mats were formed and pre-pressed using 400 mm x400 mm box. Medium density fiberboard (MDF) boards with 12 mm thickness were made by hot pressing at different specific pressures condition as shown on Table 1, at 165 –170°C press temperature. For feasibility application such waste, the average weight of Palm fronds and Palm leaves in Palm waste are estimated and recorded in Table 2.

**Table 1.** Experimental parameters.

sample code	Additives			sp. Press. (kg/cm <sup>2</sup> )
	UF (% /Substrate)	Had (% / UF)	Wax (% / substrate)	
DPF	10	1	0,5	25
SCB				25
DPF				30
SCB				30
DPF				35
SCB				35
DPF	11	1	0,5	25
SCB				25
DPF				30
SCB				30
DPF				35
SCB				35
DPF	12	1	0,5	25
SCB				25
DPF				30
SCB				30
DPF				35
SCB				35
DPF	14	1	0,5	25
SCB				25
DPF				30
SCB				30
DPF				35
SCB				35

DPF: DPF: date Palm fronds and SCB : Sugarcane bagasse

**Table 2.** UF resin specification.

Spec. Weight (kg/m <sup>3</sup> )	Solid content (%)	Viscosity (cp)	Gel time (s)	Free HCHO (%)
1275	60,55	378	68	0,18

After open air-conditioning for 24 h, these boards were cut according to standard sawing pattern into test specimens serving for the subsequent determination of basic mechanical and physical properties. Each result recorded in the following Figures is the average of five replicate measurements.

### Fiber analysis and MDF tests Chemical analysis

Parts of Date Palm rachises were subjected to mill, using sieve 250  $\mu\text{m}$  and 400  $\mu\text{m}$ , followed by conditioning in polyethylene bags for 12 hours, and labeled to be ready for work. The chemical

constituents (e.g., extractives, hollocellulose,  $\alpha$ -cellulose, lignin and pentosans) were determined by standard methods (ASTM. 2003, Wise *et al.* 1946, TAPPI T429 1998, TAPPI T222 1978, Jayme and Sarten 1940).

### **Thermogravimetric Analysis(TGA)**

The non-isothermal TGA of the selected representative adhesive systems, was carried out using Instrument SDT Q600 V20 Build 20 module (made at US), under nitrogen atmosphere at a heating rate of 10 °C/min. The analysis was carried out on adhesive casting films (~7,032- 9,40 mg), and their subjected to heat at temperature range from ~ 30 °C to 1000 °C.

#### **\*TG-curve analysis**

Kinetic studies, based on the weight loss data, were obtained by TG curve analysis. The activation energy against the appropriate order of degradation was evaluated by applying an analytical method proposed by Coats and Redfern (1964) and Basta and El-Saied 2008.

### **Differential Scanning Calorimetry (DSC)**

Differential scanning calorimetry (DSC) is the thermoanalytical technique used to measure the thermal properties of the investigated adhesive systems, as phase transition and glass transition temperature. This analysis was carried out by employing DSC on the same previous Instrument SDT Q600 V20 Build 20 DSC module (made at US), on the dynamic run, also under nitrogen atmosphere at a heating rate of 10 °C/min.

### **MDF Tests**

Different parameters of the MDF making involved different UF level (10-14%) and pressing pressure (25-35 kgf/cm<sup>2</sup>) were carried out, as shown in Table 1. The density of MDF was fixed by changing the amount of pressed fibers. The levels of UF were selected to provide MDF of E2 type with free-HCHO not exceed 27 mg/100 g board.

Three-point static bending (modulus of rupture; MOR), modulus of elasticity (MOE), and internal bond strength (IB) tests were performed in conformance with ASTM D1037-94 and ANSI A208.2-1994, for MDF panel's requirements for interior uses, using a IMAL IB500 testing machine.

For evaluating the low toxicity of the resulted composites, the perforator method (EN 120, 1992) for determination of free-HCHO in composites was carried out.

### **Statistical Analysis**

The data of the mechanical and physical properties of MDF samples manufactured from bagasse, frond, and mixed frond fibers were subjected to statistical data handling through the TWO WAY (ANOVA) variance analysis by using IBM SPSSV20 software in order to evaluate the significance of the board properties. The statistical analyses were carried out separately for both glue additions and pressing pressure.

## **RESULTS AND DISCUSSION**

### **Characterization of fibers**

The chemical analysis and average weight of Palm components were studied to examine their chemical constituents in comparison with sugar-cane bagasse, which is a commercial substrate used in local MDF mill; as well as, to estimate it's available as alternative biomass instead of bagasse. Thermal analyses (DSC and non-isothermal TGA) were carried out to examine the interaction of UF

adhesive with the foregoing agro-fibers. The importance of chemical constituents depends on the fact that, the relatively higher cellulose content may imparts the fiber strength; while the extractives will represent serious influence on the steam digestion process, and consequently MDF produced. Because, steam digestion process regards important step operation in manufacturing process, which facilitates the individualization of the fibers, and enhanced MDF formation. Moreover, the available amount of this waste for MDF production and the positive interaction between fibers and UF during resinification and curing processes are also very required for production acceptable MDF.

The results obtained are illustrated in Tables 3-6 and Figure 1 and Figure 2. Table 3 shows that, leaf of date Palm included higher extractives and lignin content together with lower cellulose and hemicellulose contents compared with Palm frond component and SCB. The higher cellulose content together with hemicellulose in case of Palm frond will play profound effect on fiber strength and self resinification of fiber during exposing to high temperature and pressure. This observation persuades us to recommend this waste in further work as precursor for production of MDF. Moreover to exclude the serious problem effect of extractives included the leaf on the machines of steam and fibrilization processes. Also, this view is emphasized from the relatively higher average weight percentages of Palm fronds (~ 57 %) than Palm leaves (43%), Table 4.

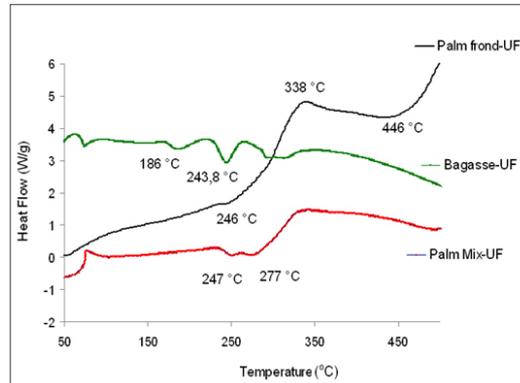
**Table 3.** Chemical analysis of date Palm frond and leaves.

Test/Material	DPR Frond	DPL Leaves	SCB Bagasse
H.Cell %	69,96	42,44	74,14
a- Cell %	38,99	22,66	42,58
Hemi %	30,97	18,78	31,56
lignin %	18,55	25,65	18,22
Pentosan %	24,79	16,65	29,22
Water Ex. %	14,16	24,24	3,97
Solvent Ex. %	1,6	4,95	1,82
Total Ex. %	15,76	29,19	5,79
NaOH %	29,26	57,79	34,5
Ash %	5,82	5,36	2,85

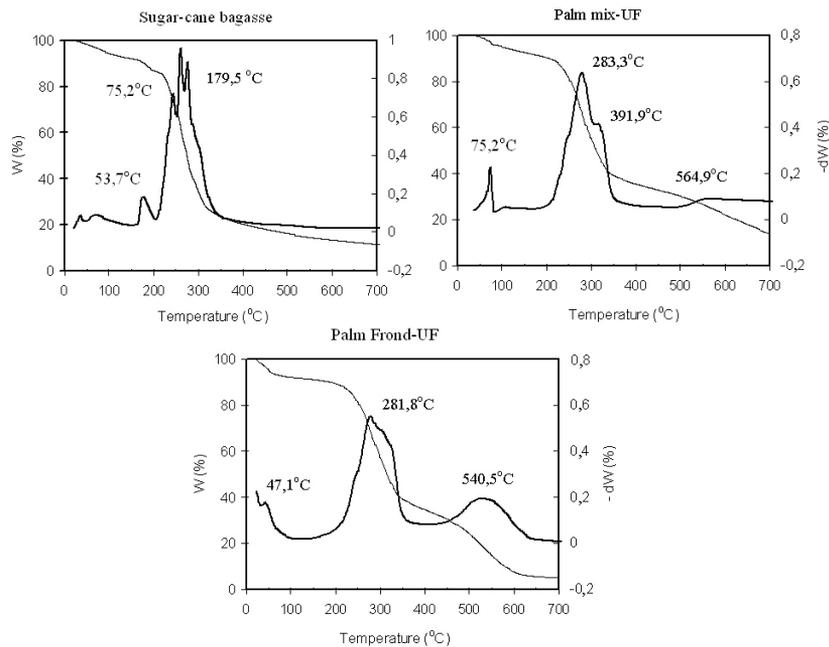
H. Cell % = holocellulose %, a-cell % = a-cellulose %, Hemi % = Hemicellulose %, Water Ex % & Solvent Ex % = water & solvent extractives % respectively, Total Ex. % = total Extractives %, NaOH % = solubility in 1 % NaOH, C.W % = Cold water solubility %.N.B. Hemicellulose content % & total Extractives can be calculated as follow Hemicellulose % = (H.Cell %) - (a-cell %) and Total Extractives % = Water Ex % + Solvent.

**Table 4.** Average weight of fresh cut date Palm components.

Test/Material	Avg. Weight	DPR Frond	DPL Leaves
Frond with leaves	2,35	1,45	0,9
Moisture content	50,00	54,00	45 %
Dry weigh	1,18	0,67	0,50
%		56,8	43,2



**Figure 1.** DSC of Palm frond fibers with UF in comparison with Bagasse fibers-UF.



**Figure 2.** Thermo-gravimetric weight loss and derivative curves of Palm frond fibers with UF in comparison with Bagasse fibers-UF.

For application in industrial scale and to reduce the effect of extractives, further study was carried out on possibility of using frond and leaves in blend, as a precursor fibrous of MDF production. To recommend the possible using blend-based fibers, its interaction with UF should be studied, in comparison with both Palm frond and bagasse fibers. In this respect DSC and TGA of Fibers-UF samples were studied.

For thermal analysis of resinated fibers, the differential scanning Calorimetry (DSC) and the non-isothermal thermogravimetric (TGA) analyses are shown in Figure 1 and Figure 2; while their calculated parameters are recorded in Tables 5 and Table 6.

**Table 5.** DSC analysis of the main Endothermic event of Bagasse- and Palm components-UF samples.

Sample	First step of curing reaction			Second step of curing reaction		
	T <sub>o</sub> (°C)	T <sub>p</sub> (°C)	rT (°C)	T <sub>o</sub> (°C)	T <sub>p</sub> (°C)	rT (°C)
Bagasse -UF	191,8	226,9	35,1	322,5	359,2	36,7
	246,9	272,0	25,1			
Palm mix-UF	238,31	248,99	10,6 8	506,62	563,22	56,60
	288,84	340,01	51,17			
Palm Frond-UF	287,39	334,54	47,15	458,41	534,70	76,29

**Table 6.** TGA kinetic parameters of Bagasse- and Palm components-UF samples.

Sample code in chart	stage	Temp. range °C	DTG peak Temp., °C	"n"	R <sup>2</sup>	SE	E <sub>a</sub> kJ/ mole	Wt. remain %
Bagasse-UF	1 <sup>st</sup>		-	-	-	-	-	94,46
	2 <sup>nd</sup>	r.t.-100,4						86,24
	3 <sup>rd</sup>	157,2-211,6	179,5	1,0	0,985	0,168	173,01	20,82
Palm Mix-UF	1 <sup>st</sup>	r.t- 106,5	75,2	-	-	-	-	94,57
	2 <sup>nd</sup>	164,8-302,7	283,3	1,0	0,988	0,1087	84,82	53,33
	3 <sup>rd</sup>	302,7-328,4	391,9	1,5	0,985	0,146	117,90	40,22
	4 <sup>th</sup>	461,3- 700,0	564,9	1,5	0,968	0,156	94,30	6,86
Palm Frond-UF	1 <sup>st</sup>	r.t- 104,33	33,7	-	-	-	-	91,97
	2 <sup>nd</sup>	150,4 - 398,5	281,8	1,0	0,989	0,125	64,18	34,74
	3 <sup>rd</sup>	398,5-651,9	540,5	0,5	0,982	0,124	124,06	5,53

With regard to DSC, Figure 1 shows that, the resinated fibers of Palm leaves and frond blend with UF exhibits three peak temperatures like bagasse- UF. While, its DSC profiles exhibit an endothermic peaks at relatively higher temperature (248,99°C, 340,01°C and 563,22°C), than bagasse-UF (226,9°C, 272,0°C and 359,2°C). The rT value of each peak, which calculated from the peak temperature and onset temperature (T<sub>p</sub>-T<sub>o</sub>), is a measure of curing rate and recorded in Table 5. Table 5 shows that the thermal curing of Palm fibers- UF behaves at lower temperatures than that of the commercial bagasse-UF. The rT value of 1<sup>st</sup> peak is about 10,68 °C for the whole Palm fibers; while in case of bagasse fiber is 35,1°C. The relatively lower value of rT in the case of blending from Palm components (Palm mix), indicates a higher rate of curing. While, in the case of bagasse-UF, curing is started at lower temperature and gives a higher value of rT, which means lower rate of curing. This trend is probably accompanied by shorting the time of penetrating the UF adhesive through whole Palm fibers, and weakness the adhesion between the fibers, due to fast the condensation of UF adhesive on fiber surface. This unaccepted trend is reduced on using Palm frond, whereas the difference values of onset temperature and peak temperature (rT) are also increased than those observed in bagasse-UF. Where, rT for the main peaks are 47,15 °C and 76,29°C; while for bagasse are 35,1 and 36,7°C.

With regard to non-isothermal thermogravimetric analysis, Figure 2 illustrates the TGA and DTG curves of the blend of Palm components (Palm mix) and Palm frond resinated fibers with UF, in comparison with bagasse fibers-UF. Table 6 summarizes their kinetics parameters. Figure 2 shows that, there are three decomposition steps for bagasse-UF and Palm frond-UF resinated fibers. The first one at temperature lower than 100 °C, indicates the evolution of adsorbed water, in addition to second

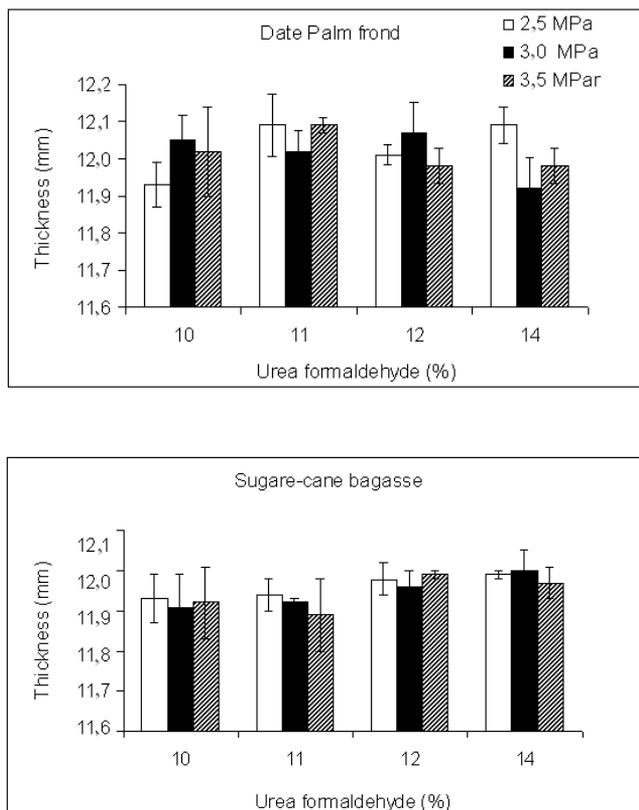
and third steps, in the ranges from 150-399 °C and 211-652 °C corresponding to volatilization and carbonization (degradation of selected adhesive systems. The ranges of degradation stages of Palm frond-UF (150,4 – 398,5°C and 398,5-651,9°C) are greater than bagasse-UF (157,2-211,6 °C and 211,6-390,5 °C). Moreover, the peak temperature of these degradation stages in case of Palm frond (281,8°C and 540,5 °C) is higher than bagasse (179,5 °C and 261,5 °C). This indicates the slowness degradation of resinated Palm frond than bagasse (higher thermal stability). This observation is in agreement with that found by DSC which supports the curing of UF on Palm frond fibers is occurred at longer time.

With regard to the blend of Palm components (leaves + frond), it is observed that the volatilization is occurred in 2 stages with DTG peaks 283,3 °C and 391,9 °C; while the carbonization stage with DTG peak at 564,9 °C. This is probably related to the relatively higher extractives included Palm leaves, which resist to some extent the role of steam and digestion process, and consequently it may affects the individualization of the fibers and interaction with UF. This extractive leads to increase the activation energy required for volatilization stage ( $\Sigma Ea = 202,7$  kJ/mole) than the case of Palm frond (64,2 kJ/mole and bagasse 173,01kJ/mole, respectively).

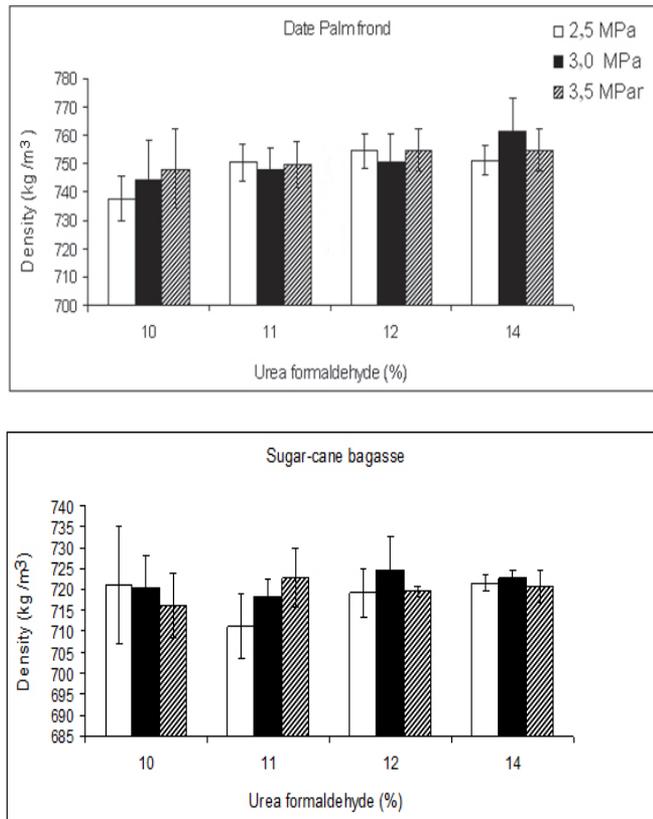
Based on the foregoing results of chemical constituents and thermal analysis, the Palm frond was candidate as substrate for MDF production. Till it possible to use as alternative to commercial bagasse, the properties of MDF made from both fibers are compared.

### Properties of MDF

The influence of preparation parameters, e.g., UF level and pressing pressure on the performance of MDF produced from Palm frond and SCB fibers are illustrated graphically in Figures 3-9.

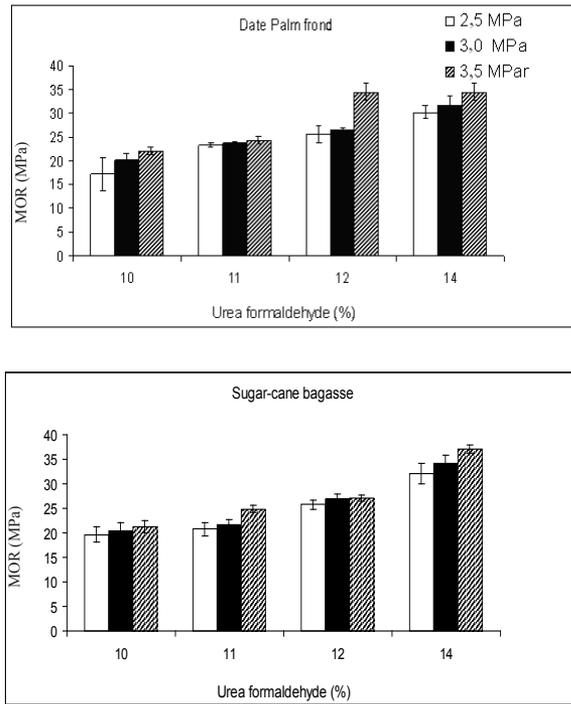


**Figure 3.** Variation of Thickness of MDF of Palm frond and Bagasse fibers versus UF %.

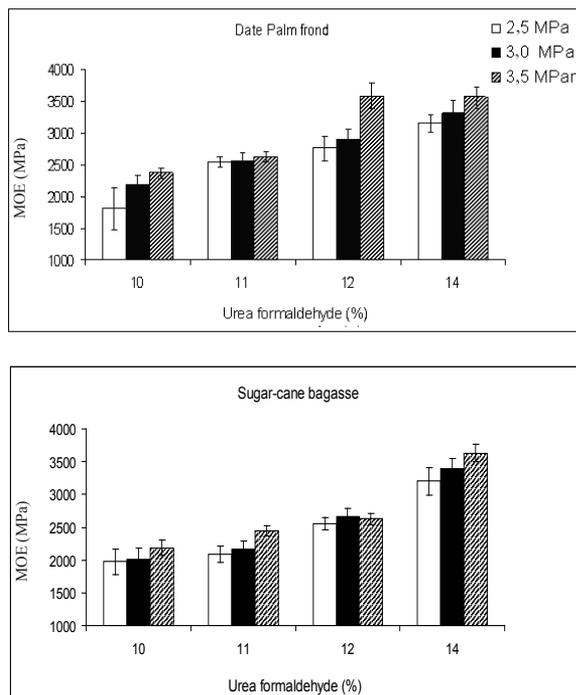


**Figure 4.** Variation of Gross density of MDF from Palm frond and Bagasse fibers versus UF % and specific pressure.

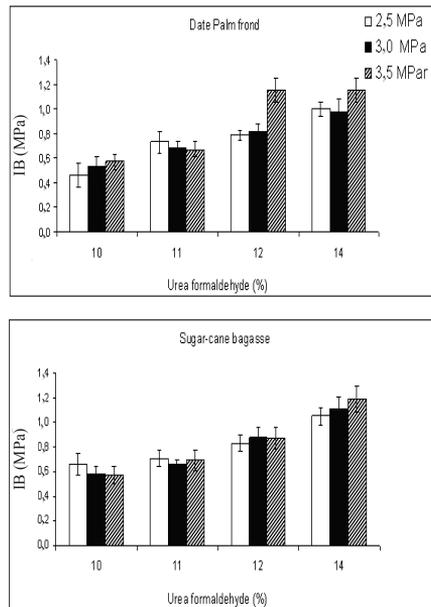
Figure 3 and Figure 4 show that, changing the UF % together with specific pressure provided board from Palm frond and bagasse with thickness ~ 12 mm; while for board density in case of Palm frond fibers is around 750 kg/m<sup>3</sup>. This value is higher than that made from bagasse (~720 kg/m<sup>3</sup>); Figure 4. Higher board density is observed in case of board made from Palm frond fibers at relatively higher UF% (14%) and applied specific pressure (3,5 MPa) (it reached 762 kg/m<sup>3</sup>). Static bending (MOR and MOE), and IB are greatly affected by changing both UF% and specific pressure (Figures 5-7). At relatively lower UF%, the specific pressure has a profound effect (improvement) on strength properties of MDF than higher ones. Where, for boards made from Palm frond fibers, at 10%UF, changing the specific pressure accompanied by increasing in MOR, from 17 MPa to 22 MPa, MOE from 1811,6 MPa to 2368,8 MPa, and IB from 0,46 MPa to 0,57 MPa. While, on applying 14%, the changes in MOR, MOE and IB with increasing the specific pressure from 2,5 MPa to 3,5 MPa are from 30 to 34 MPa, from 3153 to 3579 MPa, and from 1,0 to 1,15 MPa, respectively. A similar improvement is observed in case of SCB-based MDF. It is interesting to note that, both Palm frond and bagasse fibers at 12- 14% UF, and different specific pressure provided MDF boards fulfill the requirement of high grade MDF reported according to ANSI standard. In other words, the increasing in UF level was more significant on producing high quality MDF than specific pressure.



**Figure 5.** Variation of MOR of MDF from Palm frond and Bagasse fibers versus UF % and specific pressure.

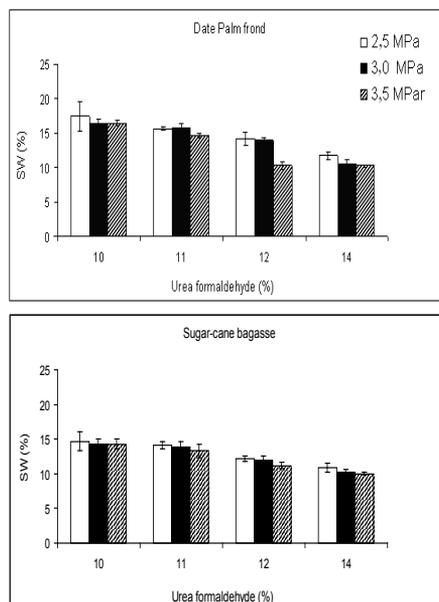


**Figure 6.** Variation of MOE of MDF from Palm frond and Bagasse fibers versus UF %, and specific pressure.

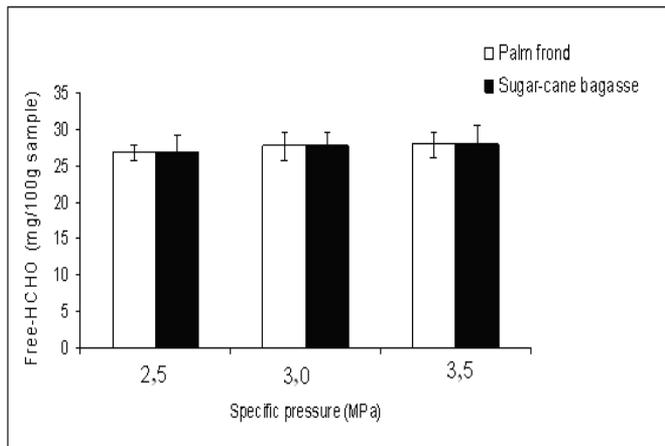


**Figure 7.** Variation of IB of MDF from Palm frond and Bagasse fibers versus UF % and specific pressure.

Results for the thickness swelling (SW) of the various MDF produced under the foregoing parameters are illustrated in Figure 8. It is clear that, the SW property of MDF decreased (improved) considerably as UF % increased from 10% to 14%. Greater reducing in this property is observed at relatively lower specific pressure (2,5 MPa), where SW decreased from 17 % to 11% and from 15% to 10%, in case of Palm frond- and Bagasse-based MDF, respectively. Increasing the applied specific pressure to 3,5 MPa, together with UF% up to 14% provides SW value ~10%, in both types of fibers-based MDF. However, the changing in pressing pressure is not significant on free-HCHO of MDF produced, where its value between 25,88 to 27,95 mg/100g board.



**Figure 8.** Variation of water swelling of MDF from Palm frond and Bagasse fibers versus UF % and specific pressure.



**Figure 9.** Free-HCHO of MDF Palm frond and Bagasse fibers versus specific pressure.

The explanation of the foregoing data may be ascribed to enhance the bond formation with increasing adhesive level and specific pressure, as well as due to the substrate constituents. Higher cellulose and hemicelluloses as well as lower extractives contents of sugar cane bagasse provide fibers easily adhered together during MDF formation, than Palm frond fibers. Higher adhesive level and pressing pressure enhancing the affinity of Palm frond fibers to response for adhering together during hot pressing.

For specifying the application of MDF produced from both fibers, as reported and based on ANSI and EN Standards, the MDFs produced from Palm frond and bagasse fibers, especially with 12-14% UF and Specific pressure 3,0-3,5 MPa have higher values than the requirements for general purposes. These boards fulfill the requirements for strength and thickness swelling properties reported in ANSI Standard. According to TS and HCHO these boards are possible for load-bearing applications and specified as E2 type boards.

The ANOVA analysis was carried out for mechanical properties and physical properties as shown, for example, in Tables 7-8. These data show a significant differences between the static bending of MDF samples made from bagasse fiber, fronds fiber, and mixed frond and frond leaves, at different addition of UF adhesive. The levels of glue addition is slightly significant on properties of MDF boards made from mixed and frond fiber than those made from bagasse, with higher specific pressure of hot press.

For economical potential of using Palm frond fibers, it will preserve the additional cost required for storage of bagasse and transportation. Moreover, this waste is available in many provinces, and persuades to construct wood Mills, without concerning on the Mills of upper-Egypt.

## CONCLUSIONS

Due to the availability of date Palm at different provinces, and for trial to minimize the economical and environmental impacts from storage of sugar-cane bagasse (SCB), as a substrate for production MDF, in this article we evaluated the Palm fibers components on the quality of produced MDF. The performance of Palm-based MDF was also evaluated, in comparison with traditional prepared SCB-based MDF. The results of chemical constituents of date Palm components (leaves and fronds), their

average weights, as well as Fibers-UF interactions (via DSC and TGA studies) lead us to recommend the use of date Palm frond (DPF) in production of MDF. DPF-based MDF especially with 12-14% UF and specific pressure 3,5 MPa have acceptable properties as compared to those produced from sugar-cane bagasse. It is static bending (MOR and MOE), internal bond strength (IB) fulfilled the high requirements in mechanical and thickness swelling properties of ANSI and EN standards. Where, their values were 34,4 MPa, 3579,2 MPa 1,15 MPa and 10,2 %, respectively.

## ACKNOWLEDGMENTS

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